

Sandy Hollow Solar Farm

Engineering Services and Civil Report

Prepared for:	Vernon Trust
Date:	9th November 2023
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Revision

Site Address: 1333 Golden Highway, Sandy Hollow, NSW
2333

Proposed Development: Solar Farm

Client: Vernon Trust

Local Authority Muswellbrook Shire Council

Authority Reference #: N/A

Stantec Reference: 301351404-SWMP_001

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Civil Project Technical Lead

For and on behalf of

Stantec Australia Pty Ltd

Revision	Date	Comment	Prepared By	Approved By
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1. Introduction

Stantec have been commissioned by Vernon Trust to prepare this Stormwater Management Plan (SWMP) in support of the Development Application (DA) for the proposed development at 1333 Golden Highway, Sandy Hollow, NSW 2333.

This SWMP illustrates that the proposed development complies with the conditions set out by Muswellbrook Shire Council, Australian Rainfall and Runoff (ARR) 2019, Australian Standards and best engineering practices.

The purpose of this SWMP is to evaluate the quantity and quality of stormwater associated with the proposed development plan so as to demonstrate that an appropriate stormwater management strategy has been adopted.

The site is situated off the Golden Highway to the south east of the Sandy Hollow Township. Adjacent to the southern boundary is railway land with the Goulburn River located further south.

The total area of the precinct is approximately 17.25 hectares and is expected to accommodate an arrangement of photovoltaic solar arrays consisting of solar panels attached to mounting structures, access roads, temporary office and set down area.

This report relates to civil development of the Sandy Hollow Solar Farm and outlines strategies associated with the provision for civil infrastructure including internal roads, stormwater drainage and earthworks.



2. Abbreviations Definitions

- **AEP** Annual Exceedance Probability
- **AHD** Australian Height Datum
- **ARI** Average Recurrence Interval
- **ARR** Australian Rainfall and Runoff
- **DA** Development Application
- **DCP** Development Control Plan
- **DN** Diameter Nominal (mm)
- **DPIE** Department of Planning, Industry and Environment
- **EY** Exceedances per Year
- **GPT** Gross Pollutant Trap
- **IFD** Intensity-Frequency-Duration
- **IL** Invert Level
- **L/s** Litres per second
- **m/s** Metres per second
- **MUSIC** Model for Urban Stormwater Improvement Conceptualisation
- **OSD** On-site Stormwater Detention
- **PSD** Permissible Site Discharge
- **RCP** Reinforced Concrete Pipe
- **RL** Relative Level
- **SID** Safety In Design
- **SQID's** Stormwater Quality Improvement Devices
- **SSDA** State Significant Development Application
- **SSR** Site Storage Requirement
- **WQO's** Water Quality Objectives
- **WSC** Water Services Coordinator
- **WSUD** Water Sensitive Urban Design



3. Relevant Policies, Standards and Guidelines

The following listed policies, standards and guidelines were referred to in the preparation of this report:

- Muswellbrook Shire Council AUS-SPEC Development Design Specifications
- Muswellbrook Shire Council Development Control Plan (DCP), 2009
- Australian Rainfall & Runoff 2019
- AS3500 parts 0-5: 2021 Plumbing and Drainage
- Landcom Managing Urban Stormwater: Soils and Construction Volume 1 2004
- NSW Floodplain Development Manual 2005
- Guidelines for development adjoining land and water managed by DECCW (OEH, 2013)

4. Existing Site Characteristics

4.1 Property Detail

The proposed development forms part of the site with the following property details:

Site Address: 511 Richmond Grove Road, Sandy Hollow,
NSW 2333

Real Property Description: Lot 12/ DP1042612

Site Area: 17.35 Ha

The proposed development can be seen on the Civil Design Documentation shown in Appendix A of this report.

The overall site is bounded by:

- Golden Highway to the North
- Gulgong Sandy Hollow Railway to the South
- Landscaped lots to the West and East

Refer to locality plan in Figure 1 for further clarification.

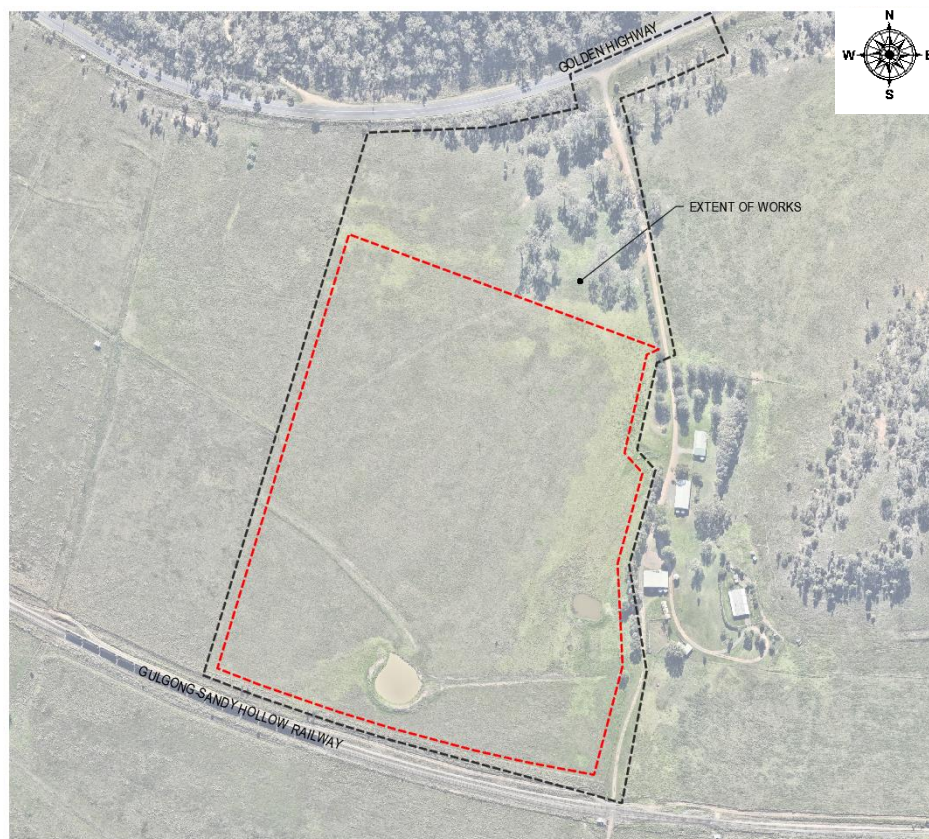


Figure 1: Site Location Plan (Source: Nearmaps 2023)

4.2 Topography

The topography of the site has been determined by analysis of survey documents and through Mecone Mosaic. The site is located to the south east of the Sandy Hollow Township and is currently used as farm land. The current site grades fall from the north east corner to the south west corner with a height range of 172.0m to RL 130.0m.



Figure 2: Sie Topography (Mecome Mosaic 2023)

4.3 Stormwater Catchments

The surrounding area has been investigated to determine the likely impact of existing external stormwater catchments on the proposed site.

Majority of the surrounding lots and roadway convey stormwater around the proposed site. There is a minor portion of stormwater from the northern lot that, in its existing condition, discharges overland toward the proposed development site. However, it is believed that little to no external catchments impact the site.

4.4 Existing Stormwater Infrastructure

Through survey information and Google Maps, it has been determined that the site does not contain pit and pipe infrastructure. The site contains two existing dams at the southern end of the site, with bund and swales running across the site to capture and direct flows into these dams.

4.5 Existing Stormwater Discharge

There is currently no formalised drainage within the site. Under existing conditions, the site drains via overland flow to the southern boundary of the site.



5. Flood Impact Assessment

When considering a new development, it is important to assess the impact of existing flooding on the proposed development and also the impact of the proposed development on existing or potential flooding both upstream and downstream of the development.

5.1 Existing Flooding

5.1.1 Regional Flooding

The subject site has been identified in the Sandy Hollow Flood Assessment (Appendix B). The site is not within the regional 100-year flood level zone, as existing levels site are above the 100-year ARI regional level of 124.4m. Therefore, it has been determined that the site is not within Flood Prone Land and is not affected by the 100-year Flood Level, as such, no flood-related development controls apply to the site.

Please refer to Flood Assessment Letter in Appendix B for further details.

5.1.2 Local Flooding

Local or Nuisance flooding describes flooding occurring due to site specific constraints. Local flooding is often caused by local topographical constraints and stormwater drainage system capacity restrictions.

Stantec have assessed the local constraints surrounding and through the site to ascertain any areas where local flooding may be an issue. The topography of the site is such that there is no risk of flooding on the site as it currently exists.



6. Earthworks and Grading

6.1 Site Grading

The proposed works on the solar farm will generally consist of minimal earthworks cut and fill operations to establish the access track and corresponding swales within the site. The two existing dams will be filled with the excavated materials from the proposed OSD/WSUD basin.

The proposed road levels are to match in with existing site grades that currently fall to the proposed basin location. Trackside swales are to follow road grades with invert depths to vary to suit draining to basin. The site is constrained by existing levels of nearby structures and existing trees.

6.2 Construction Sequence

The sequence of work for the access road construction will generally include:

- a. Provision of erosion and sediment control measures typically as outlined in section XX
- b. Inspection of exposed natural material by a qualified geotechnical engineer to ensure conformity with design assumptions and requirements; and
- c. Placement of cut to fill in layers no greater than 300mm in thickness and compacted as per the drawings.



7. Roads

The proposed road layout is based upon the concept plan approved by Vernon Trust

7.1 Design Vehicle

The design vehicle for the proposed internal roads is a 12.5m Service Vehicle which is to be used throughout the operation of the solar farm. This vehicle was used to check all turns.

7.2 Road Geometry and Width

Internal road geometry design has generally been undertaken in accordance with Council's AUS-SPEC 'Development Design Specification, 2011'.

There are 3 types of internal roads proposed for the Sandy Hollow Solar farm. Details of the internal roads are presented in the table below and are generally consistent with the works in Council's LGA.

Table 1: Internal Road Types and Widths

Internal Road Type ID	Pavement Width
Type 1	3m
Type 2	4m
Type 3	4m

7.3 Road Grading

Internal roads have generally been graded to match existing and ensure that parameters meet those presented in Council's AUS-SPEC Development Design Specification. Table 2 presents minimum, maximum and typical road grades proposed for the Solar Farm.

Table 2: Summary of minimum, maximum and typical road grades

Road Type ID	Minimum Road Grade	Maximum Road Grade	Typical Road Grade Range
All Internal Roads	0.7%	7%	4% to 6%

All internal roads have generally been designed with 3% cross fall.

7.4 Road Pavement

Preliminary internal road pavement designs have been prepared and presented in the design drawings. It should be noted that final internal road pavements are subject to further site geotechnical investigations and subgrade confirmation during construction.

Table 3: Pavement Design Summary

	Internal Road Types 1 & 3	Internal Road Type 2
Assumed CBR	3.0%	3.0%
Base	100mm	200mm



Total Pavement Thickness	100mm	200mm
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7.5 Intersection with Golden Highway

Preliminary intersection design reflecting requirements of the Traffic Impact Assessment undertaken by Amber has been included in the drawing set. Intersection design subject to review and approval by other agencies during construction certificate application.



8. Stormwater Drainage Network

8.1 Drainage Standards

The road stormwater drainage network has been designed to comply with Muswellbrook Shire Council's AUS-SPEC 'Development Design Specification, 2011' and 'Australian rainfall and Runoff, 2016'.

The proposed system will safely convey major and minor flows to the detention basin before discharging out of the site. Design rainfall intensities have been adopted from Council's Guidelines as follows:

- Minor System – 20% AEP
- Major System – 1% AEP

All overland flow paths are designed to cater for the 1% AEP storm event by maintaining a velocity-depth product of 0.4 or less and maximum flow depth equal or less than 200mm.

8.2 Catchment Area

The site is divided into 3 internal catchments and 2 external catchments. The internal catchments will drain to the proposed OSD basin for detention. The majority of the internal roads runoff will be collected by the trackside swale, then conveyed to the bioretention basins for treatment.

The external catchment to the east of the site will be captured by the swale along the boundary and bypasses the proposed OSD basin.

8.3 Hydrology Calculation

Detailed catchment modelling was conducted to calculate flows generated by the site using the Watercom DRAINS dynamic drainage modelling software. This software uses the industry standard hydrology calculation ILSAX.

The following parameters were used in the model:

- IFD Data from the ARR Data Hub;
- Depression Storage:
 - 1 mm for paved area;
 - 5mm for grassed area;
- Antecedence moisture condition 3 (rather wet);
- Time of Concentrations have been calculated within the model based on catchment size, slope and roughness.

8.4 Hydraulics Calculation

The hydraulic calculations were conducted using the Manning's Equation for the design of the road side swales.

The model represents all catchments collected via the swale network designed to cater for the minor flows with consideration to major design storms. All areas are gravity drained with overland flow in excess of swale capacity safely directed to detention basin.

There is no applicable reference to freeboard in Council's AUS-SPEC Development Design Specification. We have allowed a 150mm freeboard with the channel and road crossings have been designed for the 20% AEP.

9. On-Site Detention



An On-Site Detention basin will be provided to control stormwater discharges from the site in accordance with Council's AUS-SPEC Development Design Specification.

Hydrological analysis was conducted to determine the requirement and size of detention basins needed to reduce peak post development flows to predevelopment levels using the rainfall-runoff routing model DRAINS.

Model parameters used to determine pre and post flows are outlined in Section 6.3 of this report. A summary of peak flows from the proposed OSD basin are presented in the table below.

Table 4: OSD Basin summary of existing and developed discharge

Storm Event	Existing Peak Flow (cu.m/s)	Total Developed Peak Flow
0.5EY	0.125	0.123
0.2EY	0.326	0.161
5% AEP	0.77	0.686
1% AEP	1.48	1.48

The on-site detention system shall be sized to limit the site discharge using DRAINS to ensure post-development discharge is less than or equal to the pre-development discharge. Refer to the table below for the calculated OSD volume. This volume is based on a total site development area of 17.35Ha, a total pre-development site imperviousness of 0% and a total post development site imperviousness of 7%.

Table 5: On-Site Detention Volume

Item	Detention Volume Required (Preliminary) (m ³)
OSD	950



10. Water Quality

Water quality areas on the site have been modelled and designed in accordance with Muswellbrook Shire Council's AUS-SPEC Development Design Specification, 2011 and in accordance with, Draft Handbook Part 4: MUSIC Modelling Guide, June 2013.

Muswellbrook Council Control of erosion and stormwater management (2011) states that the main components to enhance stormwater quality are:

- Buffer zones and filter strips, being grassed, or similarly treated areas to facilitate the natural assimilation of water pollutants and reduce run-off. Refer to Buffer Zones.
- Wet retention ponds are permanent sediment ponds designed to allow particulate matter to settle out. They operate under both sedimentation and macrophyte regimes. Note that a large proportion of nutrients adhere to the sediments, and therefore settle out. Other nutrients are removed by macrophytic vegetation as part of the food chain.
- Trash Racks and Gross Pollutant Traps (GPT) designed to intercept litter and debris to maintain visual quality in downstream waterways, and to reduce the coarse sediment load on downstream water management structures.

Wetland (nutrient) filter to enhance the removal of fine sediment and nutrients from stormwater run off, and are largely dependent on biochemical removal mechanisms (i.e. nutrients taken up as part of the plant food chain).

10.1 Input Data

Water quality assessment has been undertaken using MUSIC computer software (Version 6.3.0). Catchments have been estimated from CAD base drawings with road areas assumed to be 100% impervious and the remaining catchment area pervious. Road areas were measured to calculate each catchment's total percentage impervious.

The water quality treatment train will consist of:

10.1.1 Swale/Buffer

Swales will be installed prior to stormwater discharge to the basins for catchments not bypassing bioretention areas. For catchment areas bypassing bioretention, buffer zones have been modelled prior to discharge to the basins.

10.1.2 Bioretention Areas

Two permanent bioretention areas will be provided as part of the treatment train associated with the catchments for the site. All bioretention areas will be constructed after the proposed site works have been completed and will operate as temporary sedimentation basins.

10.2 MUSIC Modelling Results

Figure 2 shows the proposed treatment train.



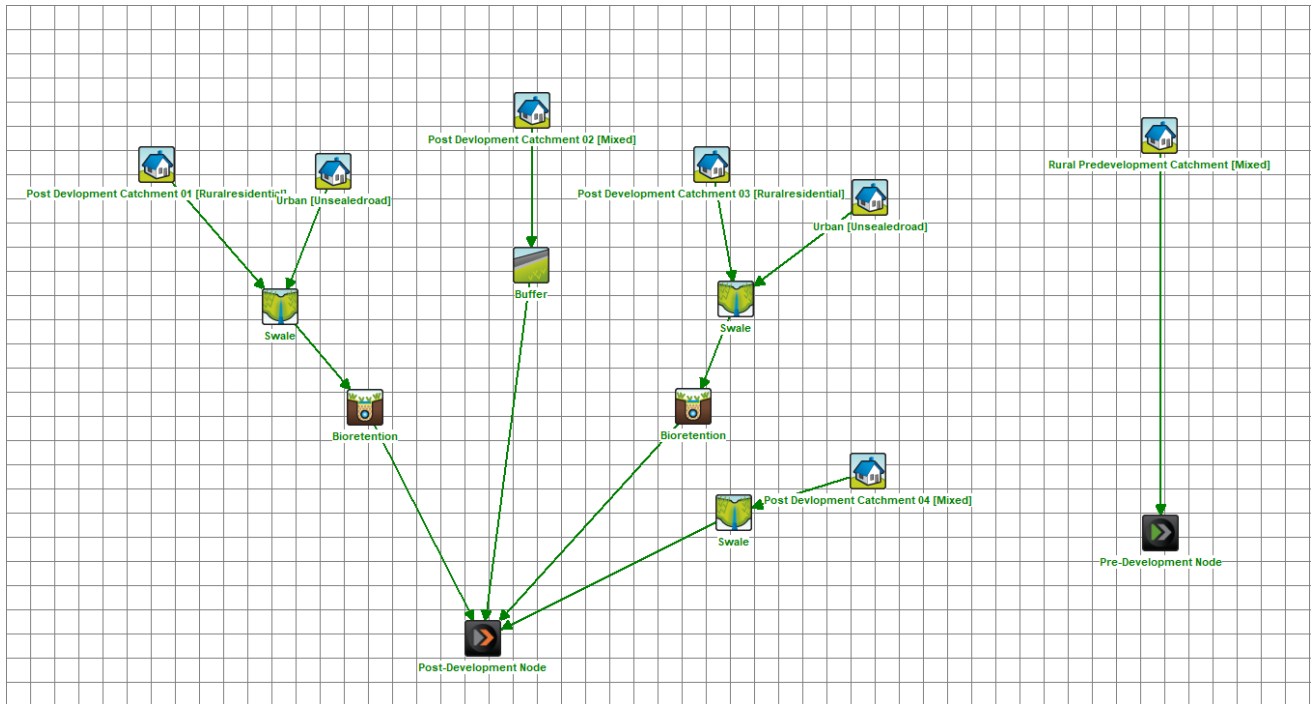


Figure 2: MUSIC Model Layout

Table 5 below presents a summary of achieved water pollutant reduction against pre-development Mean Annual Loads for the site treatment train.

Table 6: MUSIC Model Results Summary

Pollutant	Pre-Development Loads (kg/yr)	Post-Development Loads (kg/yr)
TSSⁱ	383	210
TPⁱⁱ	1.09	1.41
TNⁱⁱⁱ	9.96	13.1
GP^{iv}	0	68.3

- i. Total Suspended Solids
- ii. Total Phosphorous
- iii. Total Nitrogen
- iv. Gross Pollutants

11. Sediment and Erosion Control

Erosion and sediment control will be installed and maintained in accordance with Council's requirements and Landcom's Managing Urban Stormwater, Soils and Construction ('Blue Book').

One temporary sediment basin will be constructed as part of the bulk earthworks and maintained throughout the construction phase. The sediment basin will be located where final detention basins are proposed. The sediment basin will provide a minimum volume of approx. 3,000m³. The basin will be decommissioned as required by the construction staging.

Construction stockpiles will be located near areas of minimal cut and fill. Stockpiles will be protected above by local diversion drains and below by sediment fence.

The full sedimentation and erosion control strategy is presented in drawings 301351404-CI-070-001.



12. Conclusion

Based on the preliminary investigations, analyses and designs, it is not anticipated that any significant issues will be encountered during the detailed design of the road and drainage.

The ultimate provision of water quality measures will ensure that the water quality objectives can be achieved. The proposed OSD basin will ensure that flow rates post development will not exceed pre development rates as per Council's requirements.



Appendix A Civil Design Documentation





VERNON TRUST

SANDY HOLLOW SOLAR FARM

511 RICHMOND GROV
ROAD, SANDY
HOLLOW, NSW 2333

DA RE-ISSUE
2023.11.09

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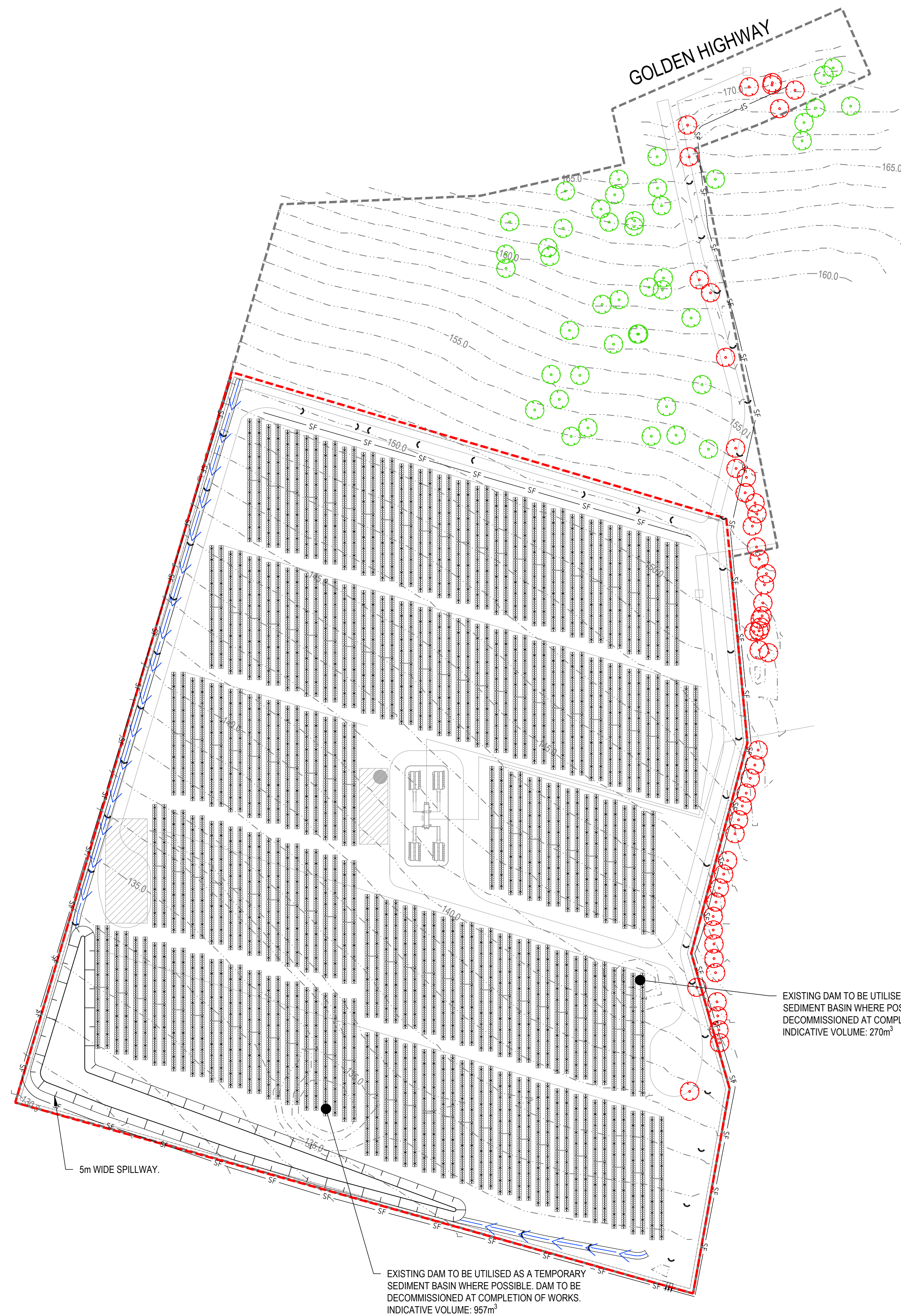
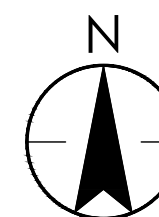
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CI-000-001	COVER SHEET, DRAWING REGISTRY AND LOCALITY PLAN
CI-007-001	GENERAL NOTES
CI-050-001	GENERAL ARRANGEMENT PLAN
CI-060-001	SITEWORKS PLAN
CI-070-001	EROSION AND SEDIMENT CONTROL PLAN
CI-076-001	EROSION AND SEDIMENT CONTROL DETAILS
CI-080-001	UTILITIES COORDINATION PLAN
CI-500-001	CATCHMENT PLAN
CI-520-001	OSD BASIN PLAN
CI-526-001	BASIN DETAILS
CI-526-101	SITEWORKS AND STORMWATER DETAILS



LOCALITY PLAN (SCALE 1:2500)

SOURCE: NEARMAP

GOLDEN HIGHWAY



LEGEND:

- SF SEDIMENT FENCE
- SBSF STRAW BALE SEDIMENT FILTER
- LS LEVEL SPREADER



Key Plan: (NTS)

A ISSUE FOR DA APPROVAL

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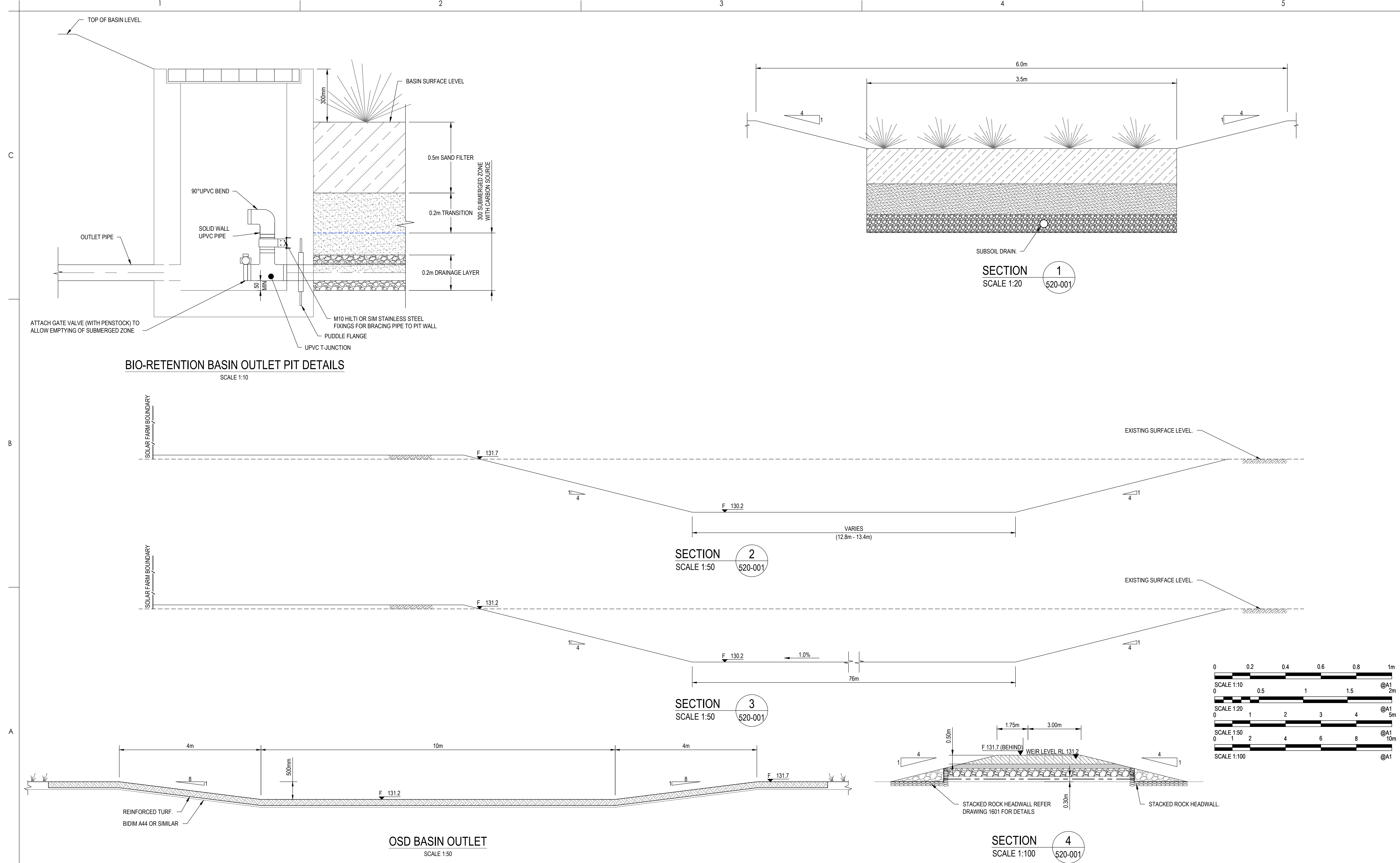
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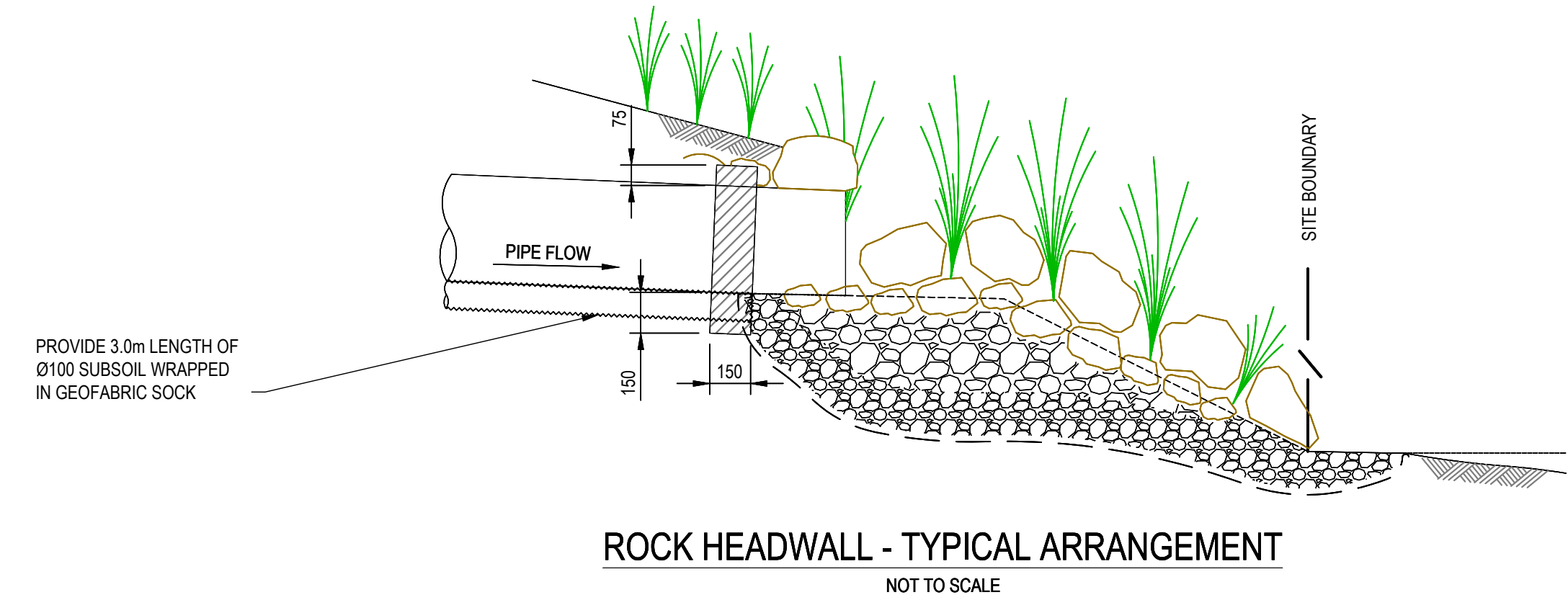
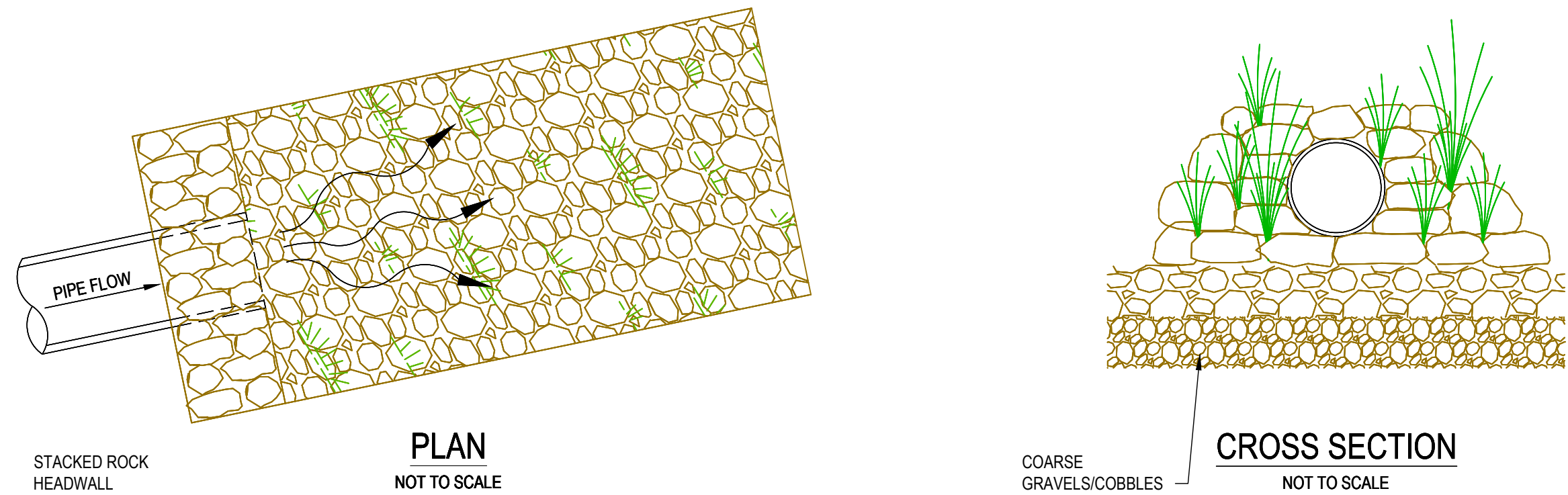
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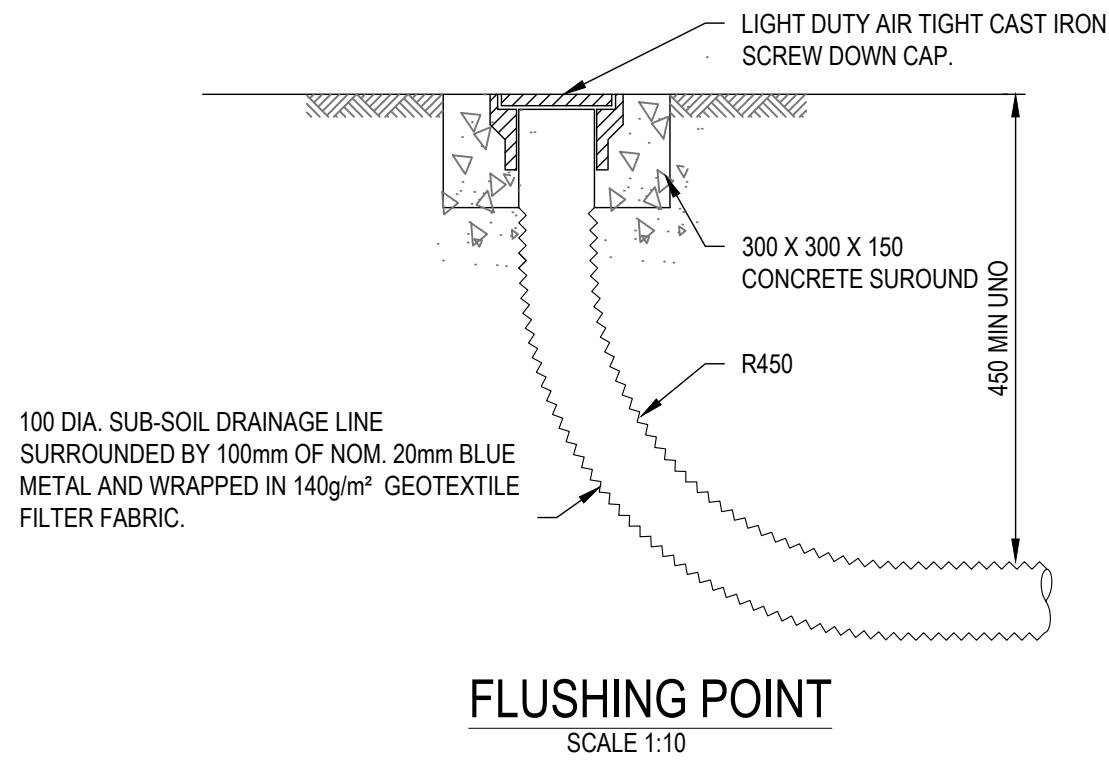


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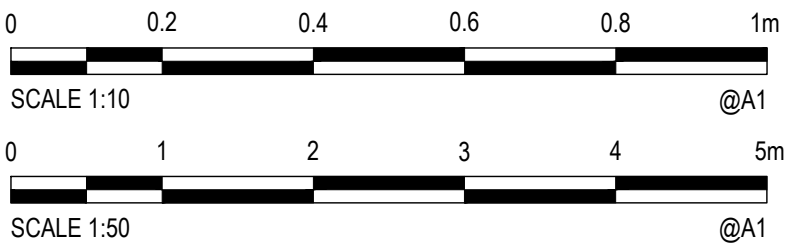
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NOTE:
SUB-GRADE FILL MATERIAL FOR TRACK TO BE OBTAINED BY CUTTING IN-SITU MATERIAL FROM V-DRAIN. TRACK SUB-GRADE LEVEL SET BY CUT TO FILL BALANCE OF TRACK AND V-DRAIN.
PAVEMENTS HAVE BEEN DESIGNED USING DESIGN SUBGRADE CBR 3%. CBR TO BE CONFIRMED ON SITE AFTER ROAD BOXING. FOR CBR LESS THAN 3%, PAVEMENT REDESIGN REQUIRED (NOTIFY SUPERINTENDENT PRIOR TO TREATMENT FOR CONFIRMATION DESIGN).



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UN301351404-PROJECT DOCUMENTATION-DRAWINGS & DESIGN SHEET SET

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Appendix B Flood Assessment



Our Ref: 80219037:AR
Contact: Andrew Reid

16 May 2019

Cardno

Attention: Rafal Piwonski

Email: rafal.piwonski@cardno.com.au

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Dear Rafal,

SANDY HOLLOW SOLAR FARM – FLOOD ASSESSMENT

The Goulburn River is located to the south of the site. We have reviewed the potential flood affectation on the site for the proposed solar farm. A 1% Annual Exceedance Probability (AEP) mainstream flood level has been estimated from available information and preliminary modelling which is sufficient for this assessment. The flood extent for an extreme event (such as Probable Maximum Flood) is not covered in this assessment.

Flood Data

Council

Council advised – “...that the site is not considered flood prone. The Goulburn River is a reasonable distance from the development site. There is no flood study for the Goulburn River and no flood mapping (either riverine or overland flow flooding) for the Sandy Hollow area. There is no further information Council can provide in this regard.”

Muswellbrook Shire Local Flood Plan (by NSW State Emergency Service, 2013)

This report lists river gauges and peak heights for historic flood events. The 1955 event is estimated to represent the 1% AEP event at the Muswellbrook and Denman gauges. The nearest gauge to the site is at Sandy Hollow about 1.5km upstream of the site (shown on the attached sketch). A flow height of 10.90m was recorded at the Sandy Hollow gauge for the 1955 event.

NSW Hunter and Central Coast Flood Summary April – May 2015 (by Manly Hydraulics Laboratory, 2015)

This report indicates a gauge zero level of 113.448 m AHD at the Sandy Hollow Gauge.

# Station	Station Name	Latitude	Longitude	Gauge Zero (m AHD)
210031	Goulburn River At Sandy Hollow	-32.3452	150.5743	113.448

Summary

Assuming the 1955 flood height at Sandy Hollow is also representative of the 1% AEP event, a flood level (1% AEP event) of 124.4m AHD is estimated. This estimate is potentially conservative as the site is downstream of the gauge.

Preliminary Flood Modelling

Simplified hydrologic and hydraulic models (XP-RAPIDS and HEC-RAS) were established for a rough estimate of the 1% AEP peak flood level in the Goulburn River. Hydrologic subcatchment data was extracted from the Hunter River Flood Study (Muswellbrook to Denman) of 2014 by WorleyParsons. Cross-sections for a 1.5km reach of the Goulburn River near the site was modelled in HEC-RAS based on LiDAR elevations.

Based on this modelling, an estimate of the 1% AEP peak flood level at the site (south-west corner) is 124.7m AHD.

Assessment

A detailed flood study of the Goulburn River is not available so an estimate of the flood extent has been compiled from available information and preliminary modelling. Based on these limitations, a peak 1% AEP flood level at the site is estimated as around 124.4 – 124.7m AHD.

The attached sketch shows an approximate extent of the 124.4m AHD and 124.7m AHD extent based on topography from LiDAR.

Survey of site by Monteath & Powys (dated 2/11/18) for the proposed solar array area (to the railway land) indicates an elevation of 129.90m AHD (at the south-western corner) to 134.1m AHD. The site is therefore considered to be several metres above the estimated extent of the 1% AEP event.

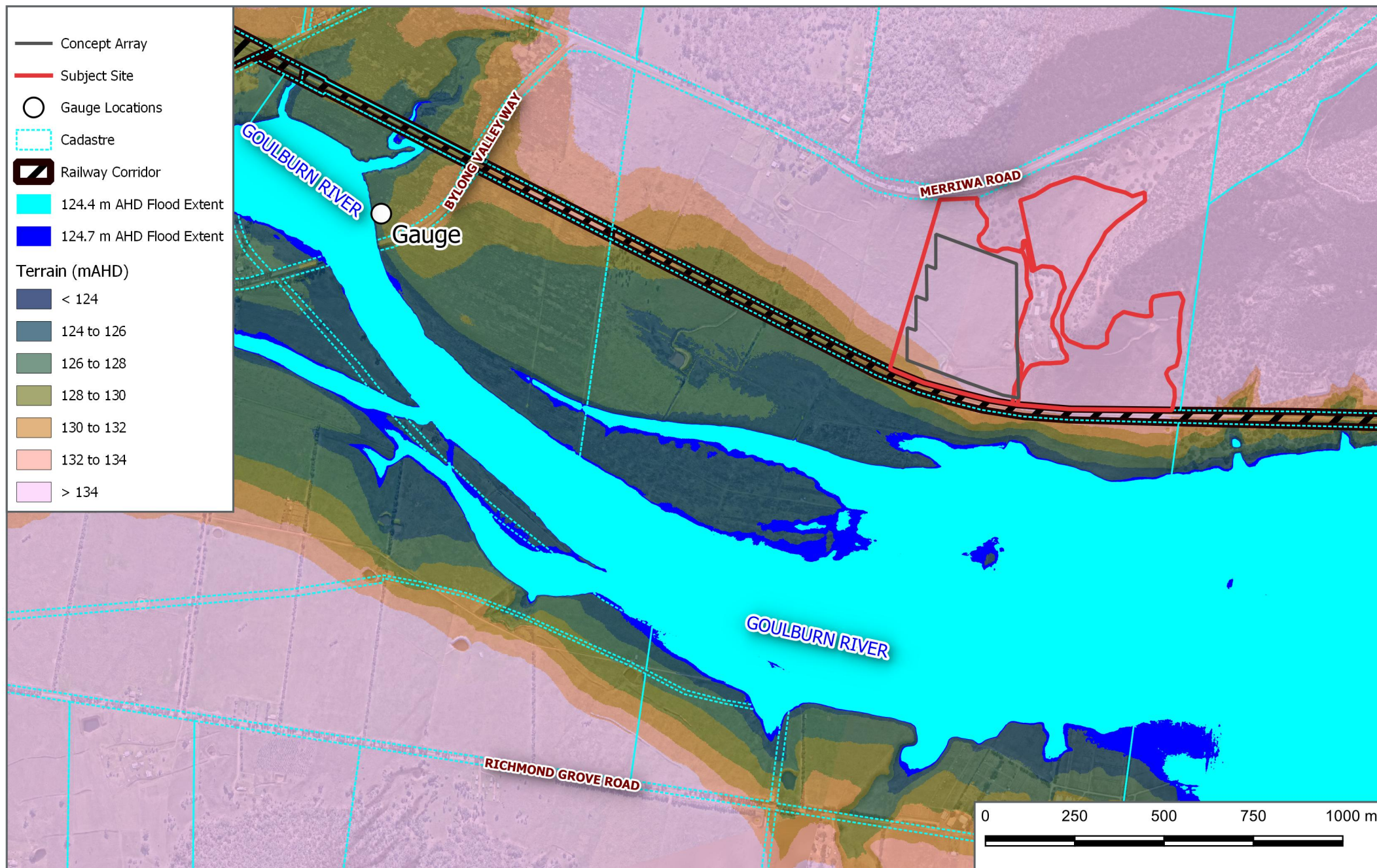
This assessment reviews potential mainstream flood inundation from the Goulburn River. Design of the solar farm on the site will need to consider potential overland flood implications from local catchments and channels on the site.

Yours sincerely,



Andrew Reid
Senior Engineer
for Cardno
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Enc: Figure showing estimated flood extent (1 page)



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